

# CADLM

Explore new industrial horizons

Optimal Decision Support System for Engineering and Expertise

**La réduction de modèles : une solution efficace pour la modélisation paramétrique, optimisation et analyse de la robustesse**

**Model reduction : An efficient solution for parametric analysis, optimization, robustness and reliability analysis**

Kambiz Kayvantash : [kambiz.kayvantash@cadlm.com](mailto:kambiz.kayvantash@cadlm.com)

# CADLM: Transforming data into intelligence

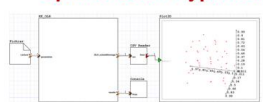
- **Crash/Safety/Biomechanics**
- **Complex systems optimization**
- **Robustness and Reliability analysis**
- **AI, Data mining, Data fusion**
- **Reduced modelling**



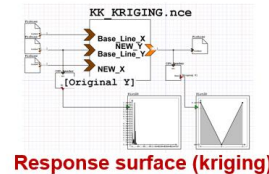
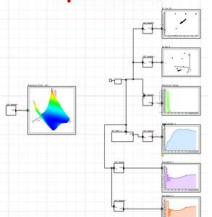
**Customized solutions & software**

# ODYSSEE

## Sampling Optimal Latin Hypercube

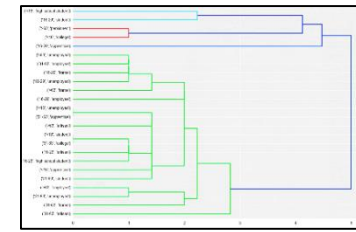
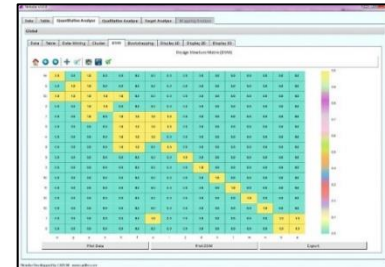


## Optimization

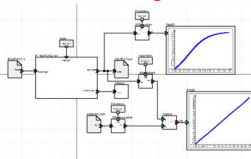


## Response surface (kriging)

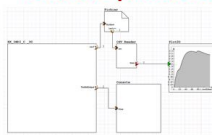
	Epaisseur	Diamètre	Longueur	Masse
Epaisseur	1.000	0.400	-0.096	0.808
Diamètre	0.400	1.000	0.077	-0.903
Longueur	-0.096	0.077	1.000	0.940
Masse	0.808	-0.903	0.940	1.000



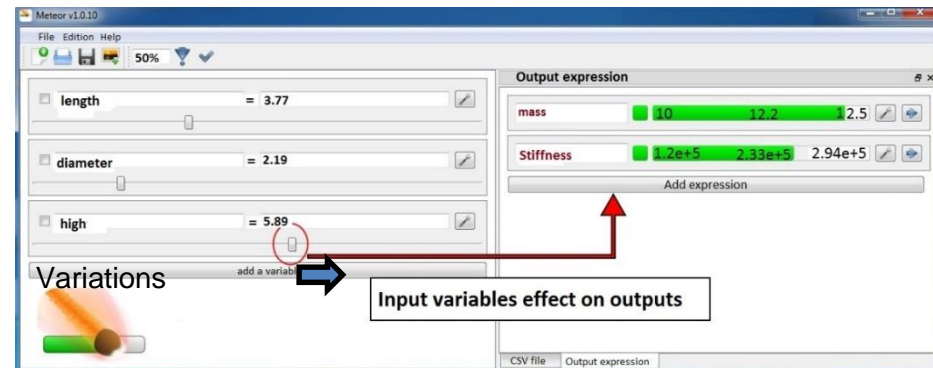
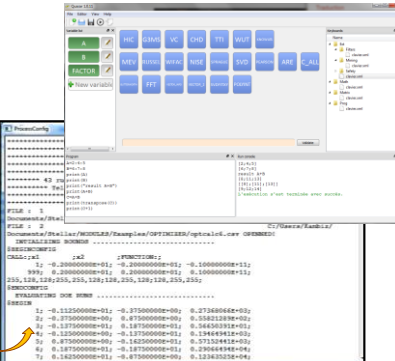
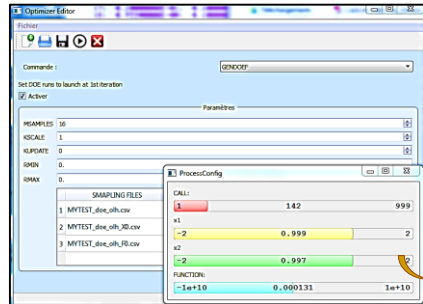
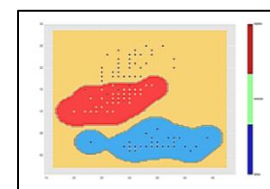
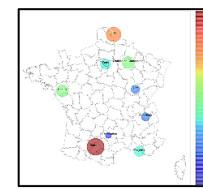
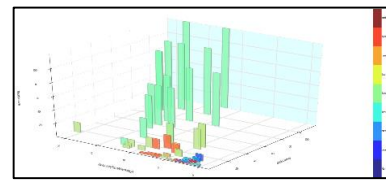
## Virtual Testing



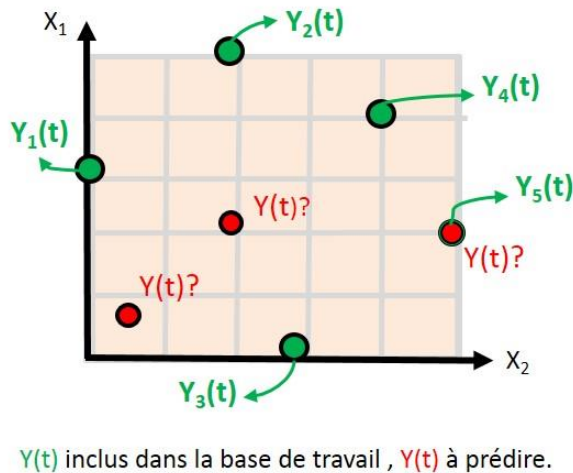
## Robust Optimization



## Model Reduction



# ODYSSEE



**Optimisation rapide des systèmes  
physiques et numériques  
grâce à la prédiction instantanée  
(application embarquée)**

**Predicting impact of new parameter sets without FE computing or additional experiments.**



# Model Reduction

## (ROM=Reduced Order Modelling)

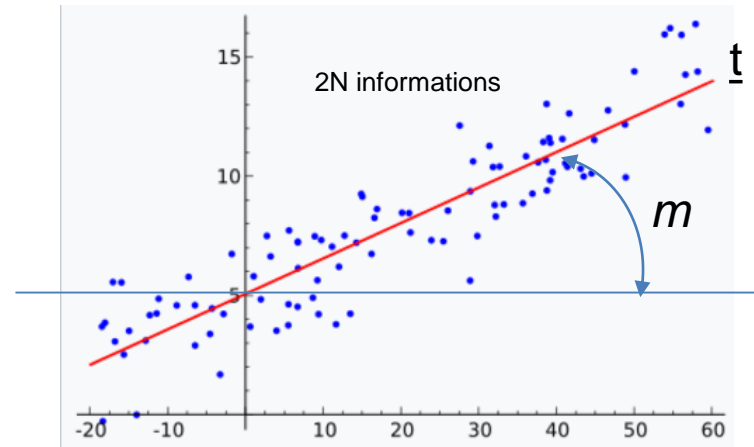
- Introduction on Modal Decomposition
- PGD (Proper Generalized Decomposition)
- Hyper-Reduction
- **POD (Proper Orthogonal Decomposition)**
- Reduced basis methods, Polynomial Chaos (Lagrange, Hermit, Taylor)
- **CVT (Centroidal Voronoi tessellations)**
- **Applications Crash/Safety**

# Example - Equation of straight line

Slope, intercept :  $y = m x + b.$   $m = \frac{y_2 - y_1}{x_2 - x_1}$  ➡ 2 or 5

Point, intercept :  $y - y_1 = m (x - x_1).$  ➡ 3

General form  $a x + b y + c = 0.$  ➡ 3



Parametric form

$$\begin{aligned} x &= x_1 + t \\ y &= y_1 + m t \end{aligned}$$

Each value of  $t$  gives a different point on the line.

➡ 3

(eigenvalue -> eigenvector)

# Example - Equation of straight line

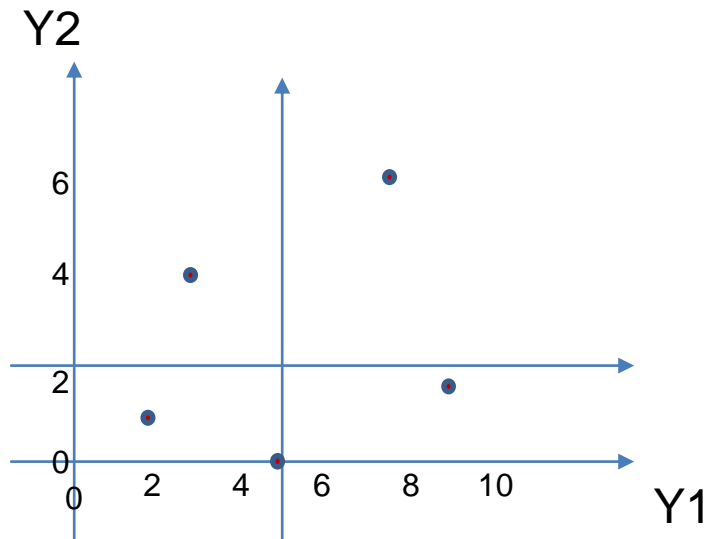
Parametric form

$$\begin{aligned}x &= x_1 + t \\ y &= y_1 + m t\end{aligned}$$

Each value of  $t$  gives a different point on the line.

- Information is reduced/ regressed / fusioned
- Instead of  $2N$  data we need only need  $N+4$  ( $\underline{t}_N, m, x_1, y_1$ )
- $\underline{t}$  is an **eigenvector** and  $m$  is an **eigenvalue**
- We can reconstruct (approximately) **X** and **Y** knowing only  $\underline{t}$  and  $m$  !

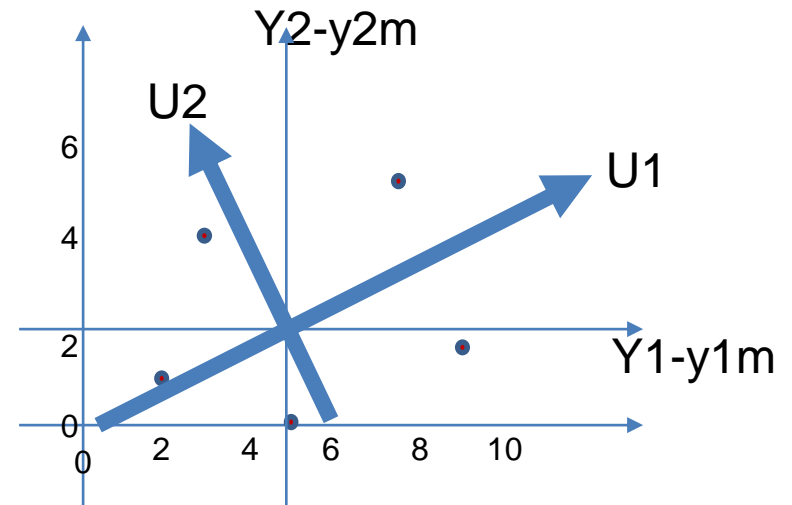
# PCA



$Y =$

2 ; 1  
3 ; 4  
5 ; 0  
7 ; 6  
9 ; 2

Strong coupling



$Y =$

-3.578 ; 0  
-1.342 ; 2.236  
-1.342 ; -2.236  
3.130 ; 2.236  
3.130 ; -2.236

Weak coupling



# Modal Analysis

$$M\ddot{a} + C\dot{a} + Ka + f = 0$$

Strong coupling

$$a = \bar{a}e^{\alpha t} = \sum_{i=1}^n \bar{a}_i e^{\alpha_i t}$$

Transformation

$$m_i \ddot{y}_i + c_i \dot{y}_i + k_i y_i + f = 0$$

Weak coupling

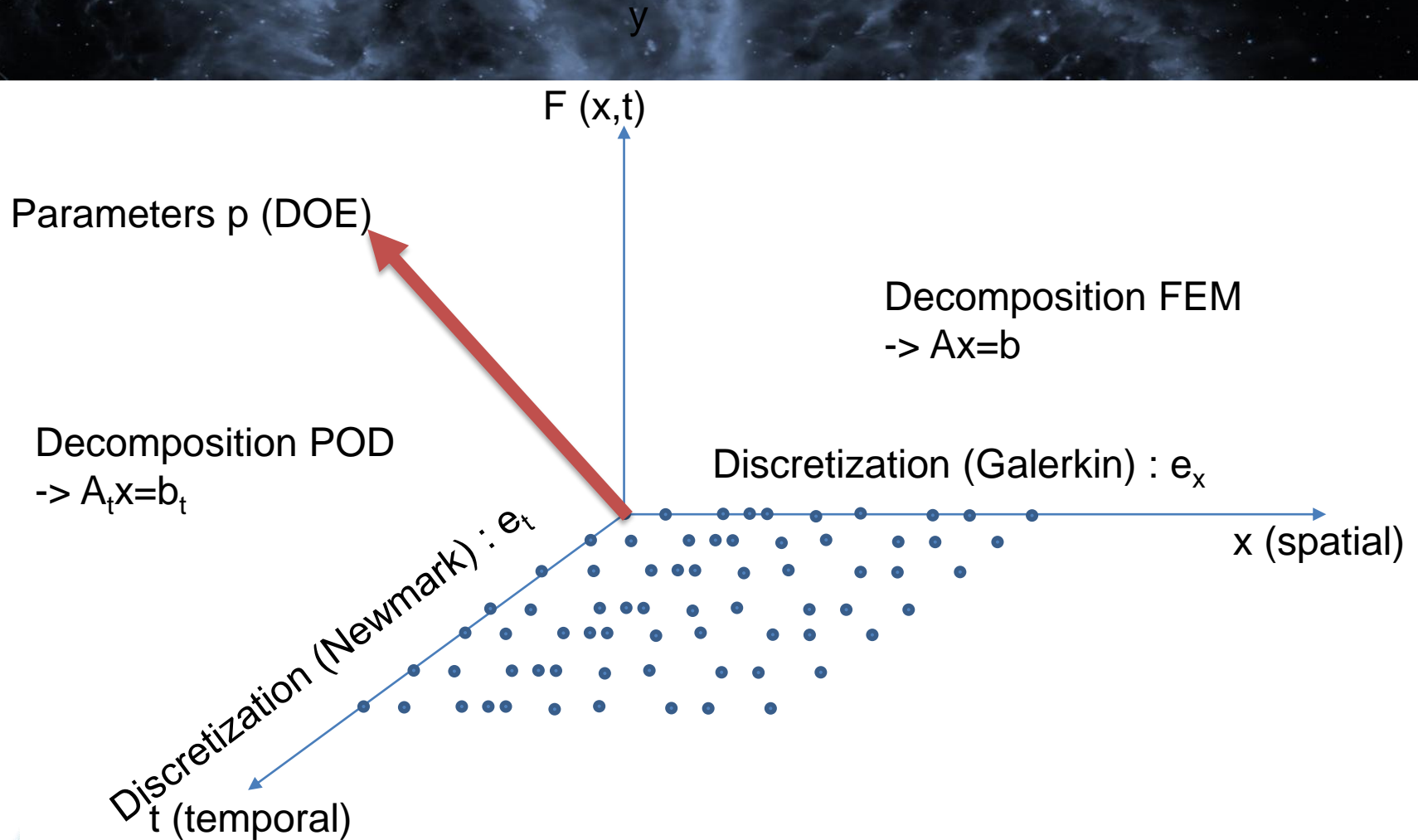
$$m_i = \bar{a}_i^T M \bar{a}_i = 1 \text{ (if modes are normalized)}$$

$$c_i = \bar{a}_i^T C \bar{a}_i$$

$$k_i = \bar{a}_i^T K \bar{a}_i$$

$$f_i = \bar{a}_i^T f$$

# FE versus ROM



# Model reduction techniques

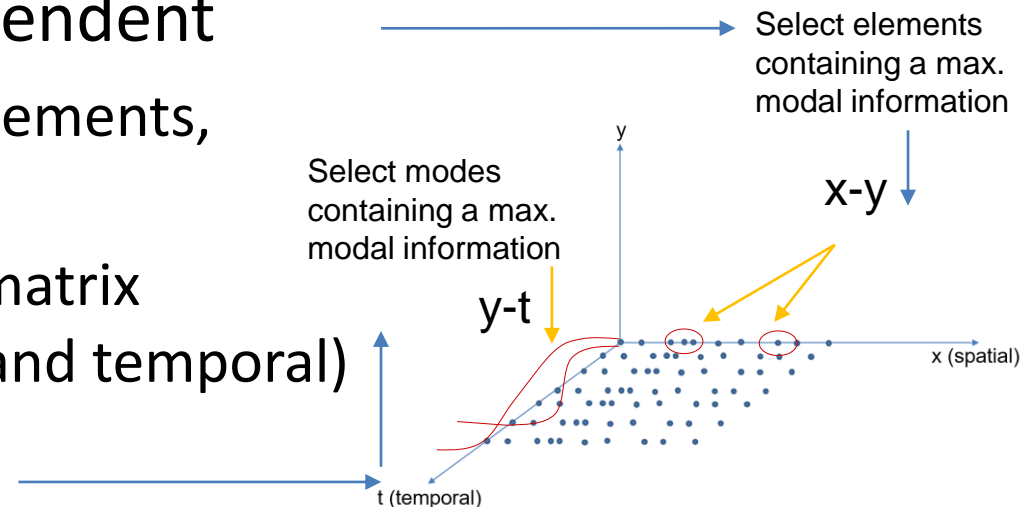
- **Intrusive**

- A priori, Solver dependent

- Shape functions (elements, spatial)
    - Reduced stiffness matrix (elements, spatial and temporal)

- **Non-Intrusive**

- A posteriori, post-processing



# PGD (Proper Generalized Decomposition)

- **PGD (proper generalized decomposition)** is an approximation of the weak solution of parametric FE model
- Construction of tensorial formalism of the Newmark equations for whole of time domain at once in order to obtain a new system of linear equations
- Separation of variables in spatial and temporal modes
  - $Y(x,t) = \sum G(x) \cdot H(t)$
- Application of time-series approach in temporal domain (iterative)

$$\Rightarrow x(t, \Delta) = \sum_{i=1}^{\infty} \Phi_i(\Delta) \mathcal{X}_i(t) \quad (1)$$

where  $\Phi_i(\Delta) \in (\mathbb{R}, \mathcal{B}(\mathbb{R}))$ , and  $\mathcal{X}_i(t) \in \mathbb{R}^m \forall i = 1, \dots, n$ .  
If we truncate the sum to  $N$  terms, we have,

$$x^N(t, \Delta) = \sum_{i=1}^N \Phi_i(\Delta) \mathcal{X}_i(t), \quad (2)$$

In PGD framework, the sum  $x^N(t, \Delta)$  is constructed incrementally by solving for the functions  $\Phi_i(\Delta)$  and  $\mathcal{X}_i(t)$ . We assume that the sum given in (2) is known upto  $n < N$  terms. Next we introduce a candidate  $n + 1^{\text{th}}$  term such that

$$x^{n+1}(t, \Delta) = x^n(t, \Delta) + P(\Delta)Y(t). \quad (3)$$

where  $P(\Delta) \in (\mathbb{R}, \mathcal{B}(\mathbb{R}))$  and  $Y(t) \in \mathbb{R}^m$  are unknown functions. The couple  $P(\Delta)$  and  $Y(t)$  is known as the *enrichment couple*. We then solve for  $P(\Delta)$  and  $Y(t)$ . This *enrichment procedure* continues until,

$$\|x^{n+1}(t, \Delta) - x^n(t, \Delta)\| < \epsilon$$

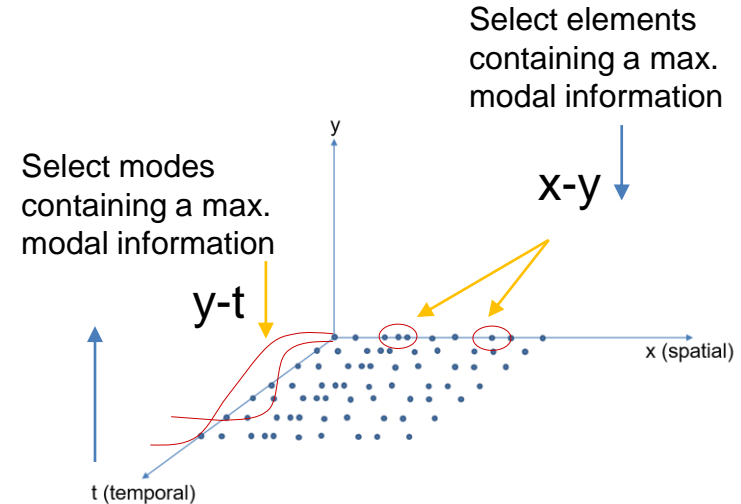
See also Chinesta et al.

Reduced Order Modeling for Systems with Parametric  
Uncertainty Using Proper Generalized Decomposition  
Parikshit Dutta

# Intermediate methods

- **Hyper-reduction**

- An adaptive modification of the base as we go on (in time) which necessitate a new basis reconstruction
- Adaptive meshing (use POD between two re-meshing FE steps) an initial DOE anyway (Full FE) -> POD ? (needs initial basis)



See also David Ryckelynck



# POD

## for on-board and real-time computing

- **POD (Proper orthogonal decomposition)** are algebraic approximation solutions allowing for fast (real-time) interpolations
- **Reconstructions or extrapolations** based on previously existing DOE-type results (snapshots) obtained either from FE computations or directly from experimental results
- **Unlike response surface methods** where smoothed solutions on certain criteria are obtained, **POD provides complete solutions** (reconstructions) of the space-time response of the original differential equation.

$$F(x,t) = G(x) \cdot H(t)$$

# POD

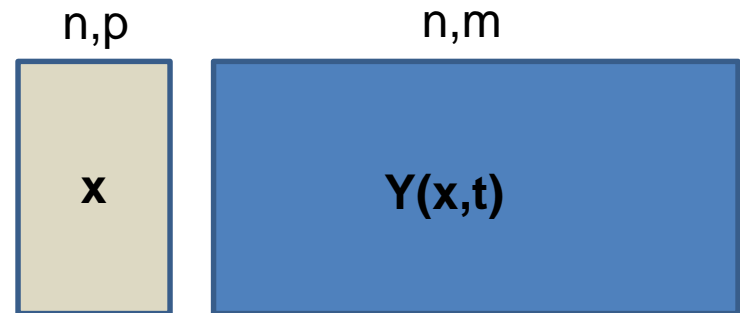
- Let  $X \{x_1, \dots, x_p\}$  and  $Y \{y_1, \dots, y_m\}$
- Assume  $y_k = \hat{A} x_p \rightarrow \text{find } \hat{A} ; (p \leq m)$
- Decompose  $Y_{n,m}$ 
  - If  $m \gg n \rightarrow$  **Direct method (SVD)**
  - If  $m \ll n \rightarrow$  Snapshots method (Correlation Matrix)

$$M\ddot{a} + C\dot{a} + Ka + f = 0$$

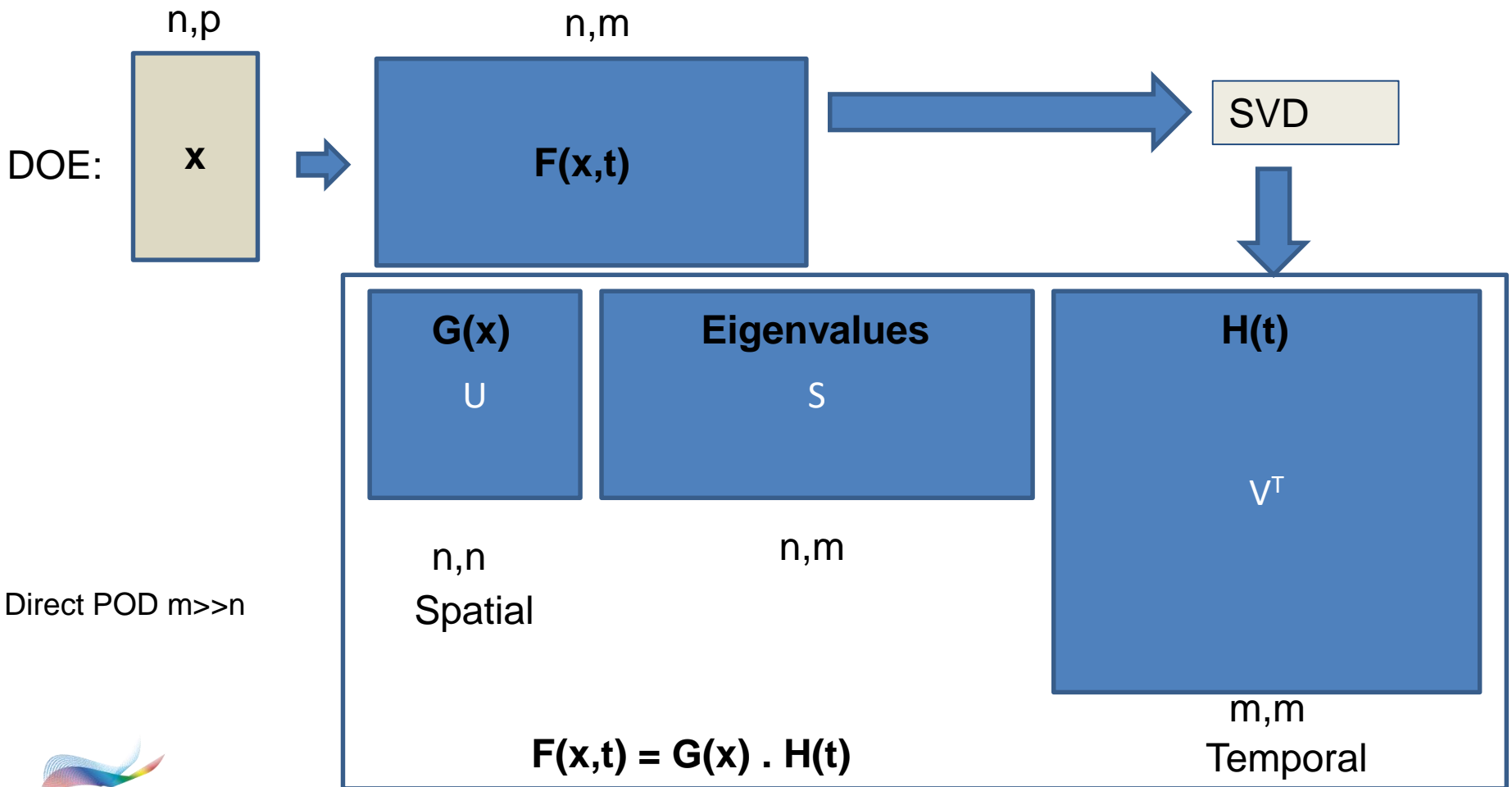
↓

$$a = \bar{a}e^{\alpha t} = \sum_{i=1}^n \bar{a}_i e^{\alpha_i t}$$

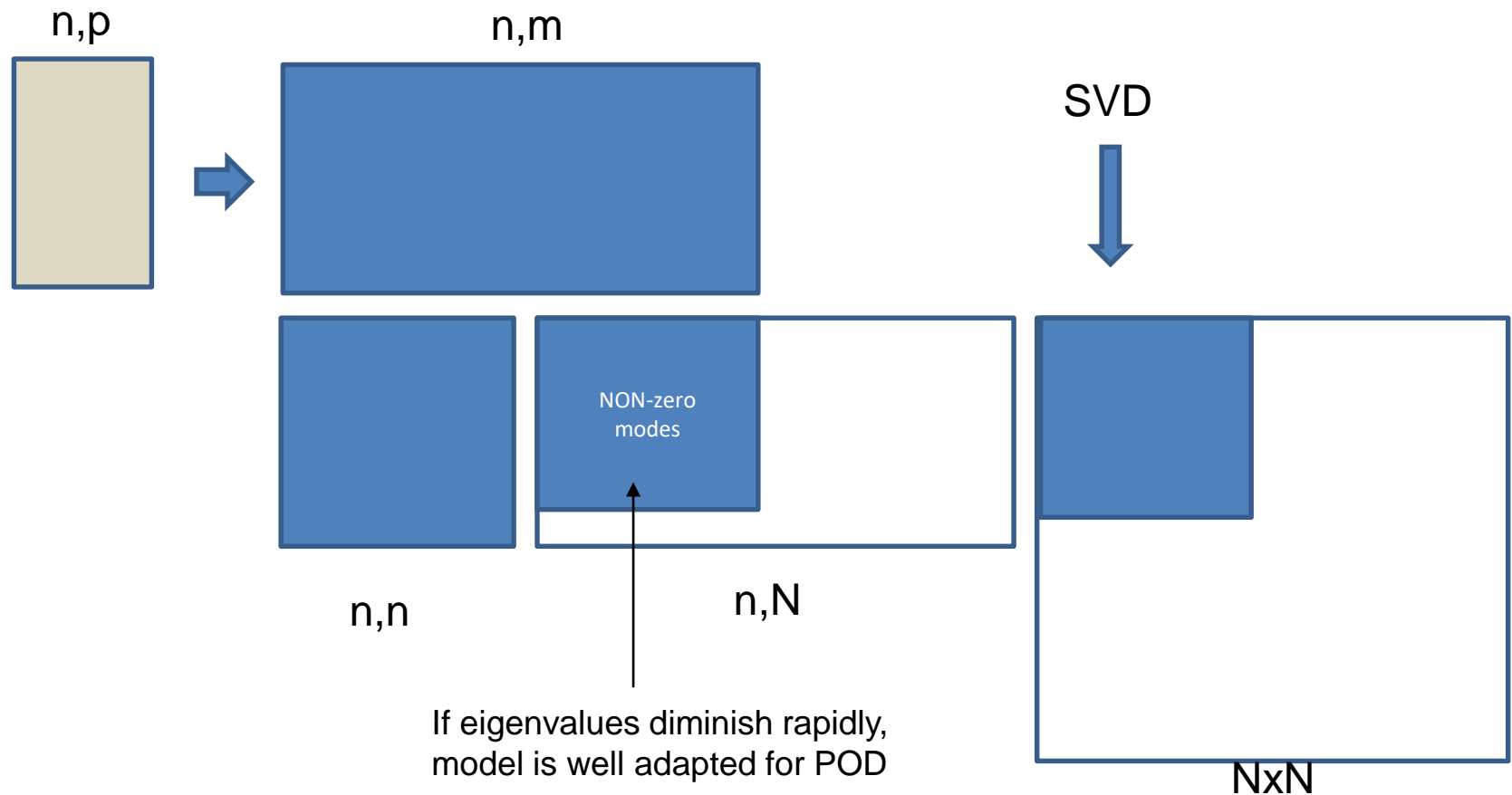
Modal basis  
(c.f. PCA)



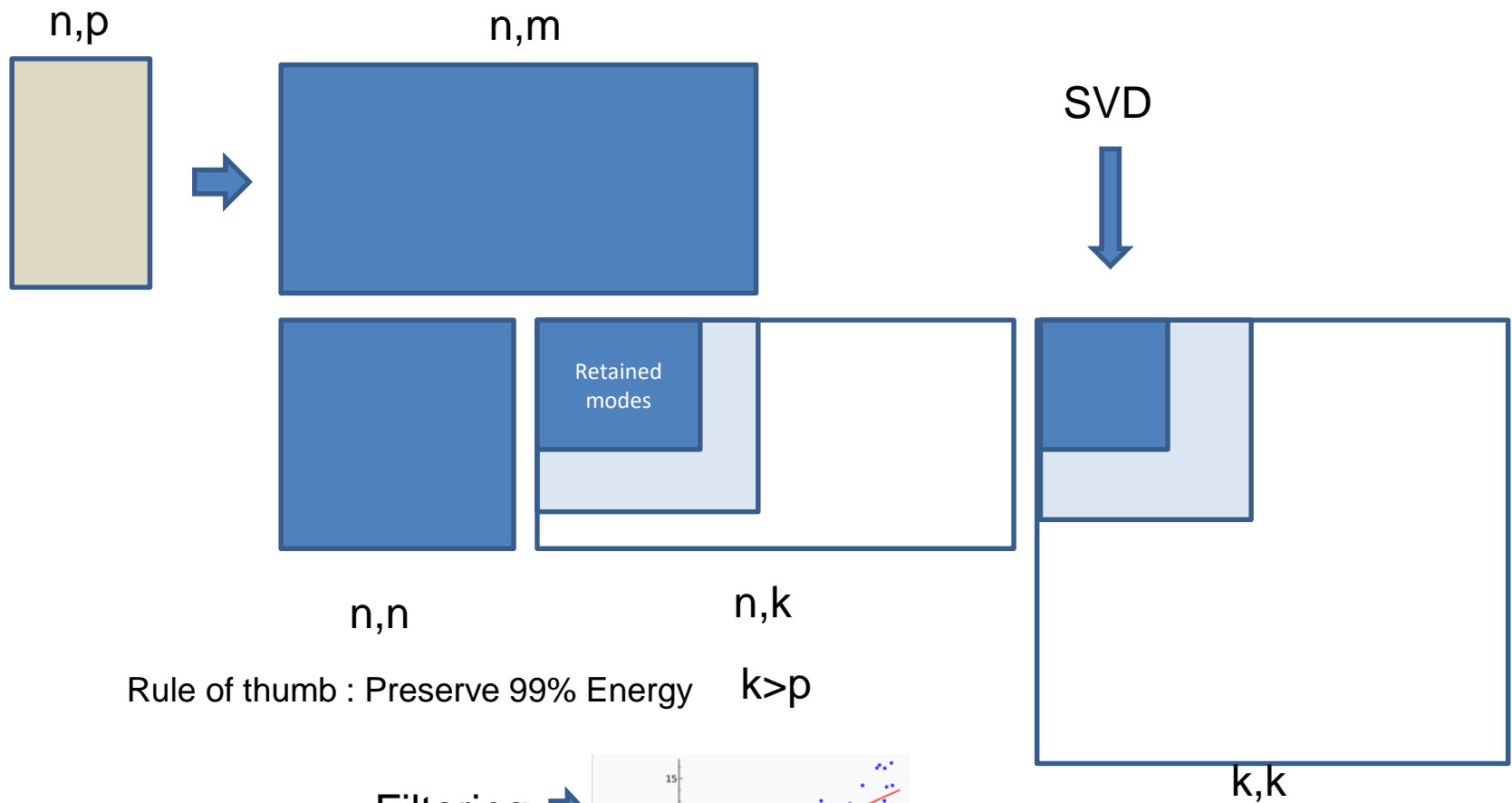
# Singular Value Decomposition



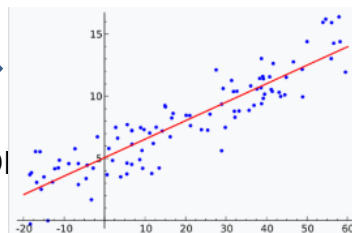
# Singular Value Decomposition



# Singular Value Decomposition



Filtering →





# Summary of a POD algorithm

1) EF  $\rightarrow \mathbf{Q}(\mathbf{x}, t) \quad (t_0 < t < t_N)$

2) DOE  $\rightarrow \mathbf{x}_{(n, p)} : \mathbf{Q}_{(n, m)}$

3) SVD  $\rightarrow \mathbf{Q} = \mathbf{U}_{(n, n)} \mathbf{S}_{(n, m)} \mathbf{V}^T_{(m, m)}$

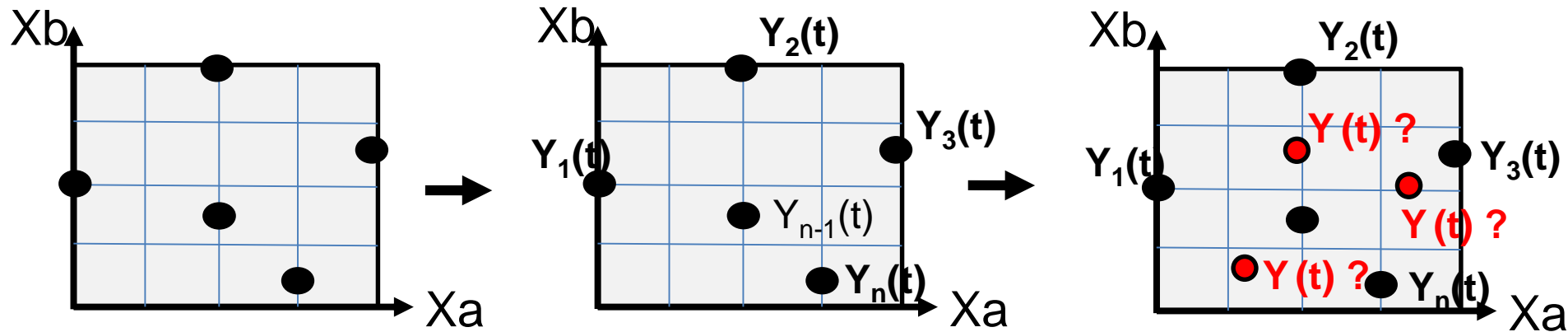
4) RDA  $\rightarrow \mathbf{x} \mid \mathbf{U} \mathbf{S} \quad (O(\mathbf{x}) = \mathbf{q}(\mathbf{x}))$

5)  $O(\mathbf{x}_{\text{new}}) \rightarrow \mathbf{q}_{\text{new}}$

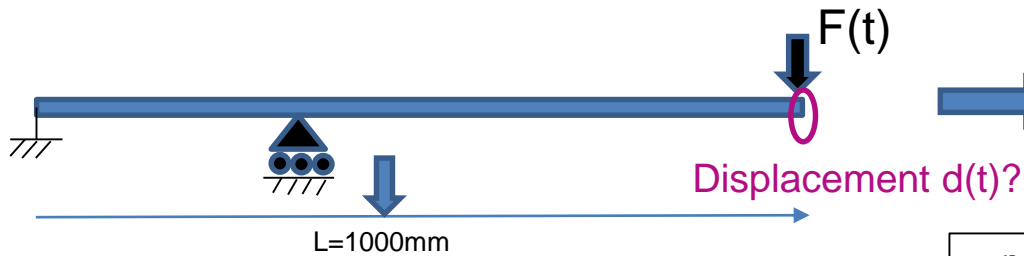
6)  $\mathbf{q}_{\text{new}} \cdot \mathbf{V}_T = \mathbf{Q}(\mathbf{x}_{\text{new}}, t_N)$

Know-how

# How it works



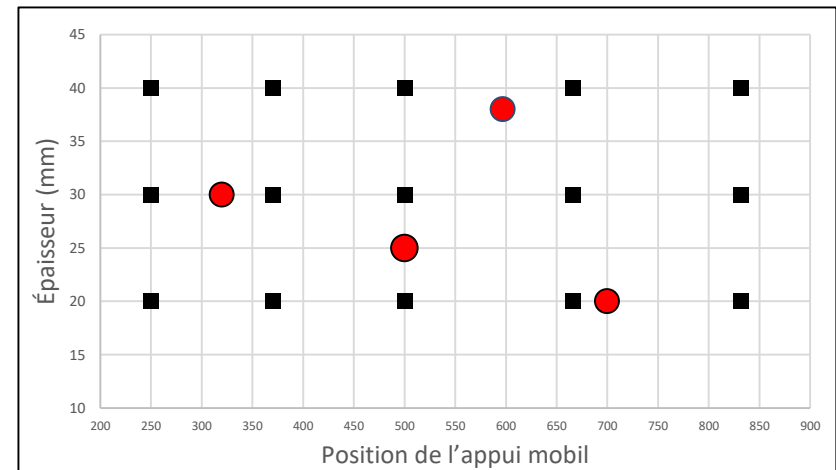
# Example – plate flexion



Influence lines

CADLM - flexion planche - X1:épaisseur=35mm - X2:Distance appui mobile=4  
Time = 0  
Contours of Effective Stress (v-m)  
max IP, value  
min=0, at elem# 1  
max=0, at elem# 1

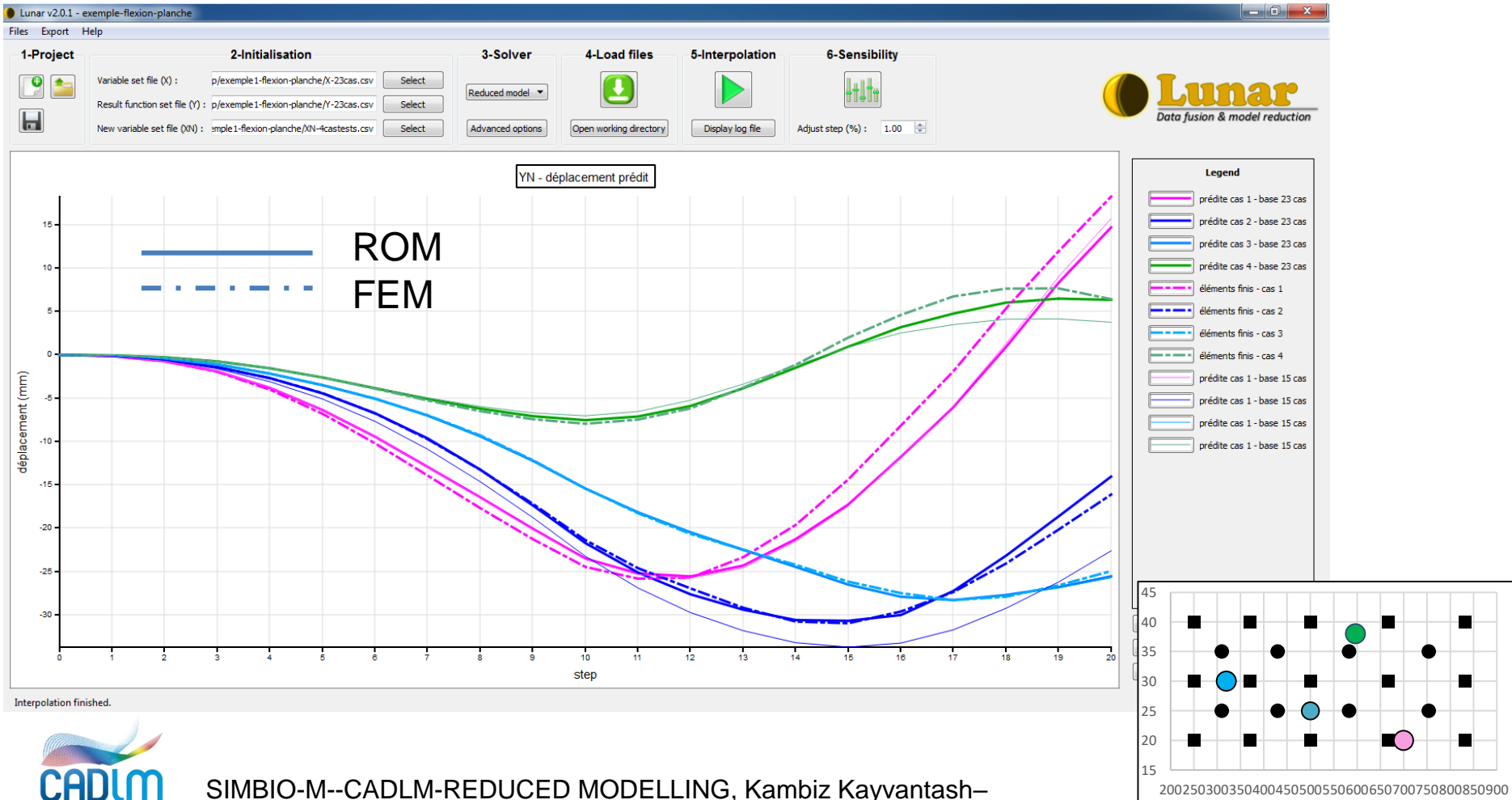
Fringe Levels  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00



Model parameters  
X1: plate thickness  
X2: mobile support distance

Predict: Y: displacement-time over the complete spatial domain

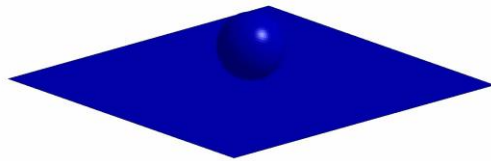
# Example – plate flexion



# Example – plate impact

CADLM - flexion plaque  
Time = 0  
Contours of Effective Plastic Strain  
max IP value  
min=0, at element 1  
max=0, at element 1

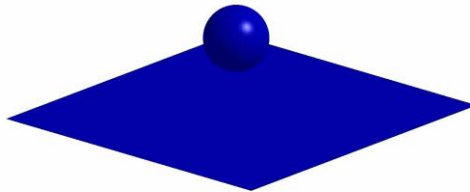
Fringe Levels  
0.000e+00  
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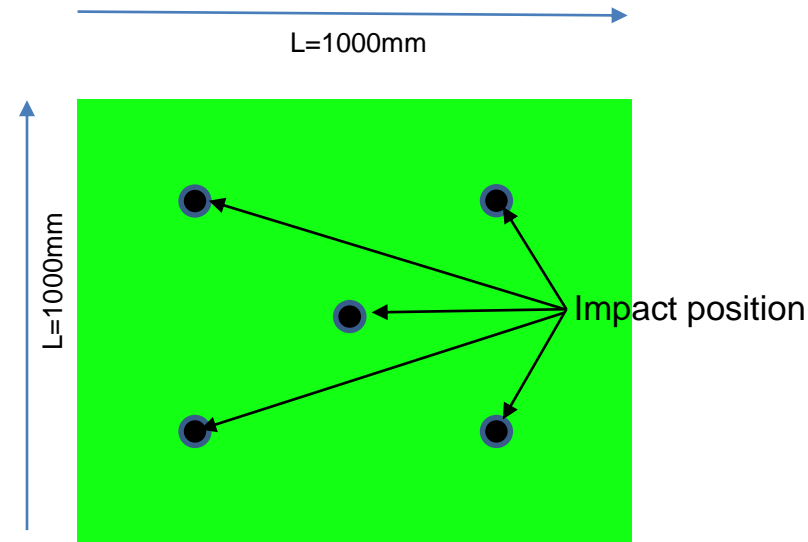
Without rupture

CADLM - flexion plaque  
Time = 0  
Contours of Effective Plastic Strain  
max IP value  
min=0, at element 1  
max=0, at element 1

Fringe Levels  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
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0.000e+00  
0.000e+00



With rupture



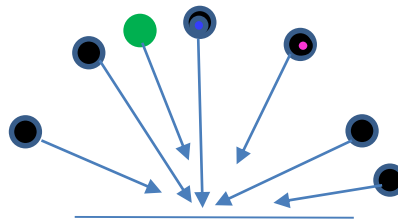
Model parameters:  
X1: impactor velocity  
X2: impact position  
X3: impact angle

Predict:  
Y: internal energy  
Y: impact force

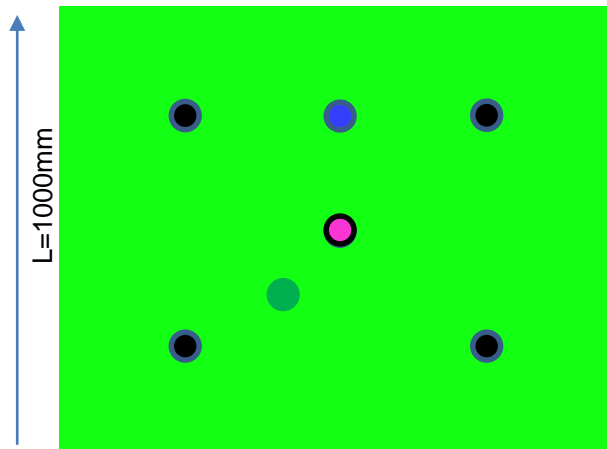


# Example – plate impact

Model parameters:  
X1: impactor velocity  
X2: impact position  
X3: impact angle



(mm/s)	V1	V2	V3	V4
DOE	5000	7500	8750	10000
Test	6000	7500	9000	



**Test 1** : New velocity

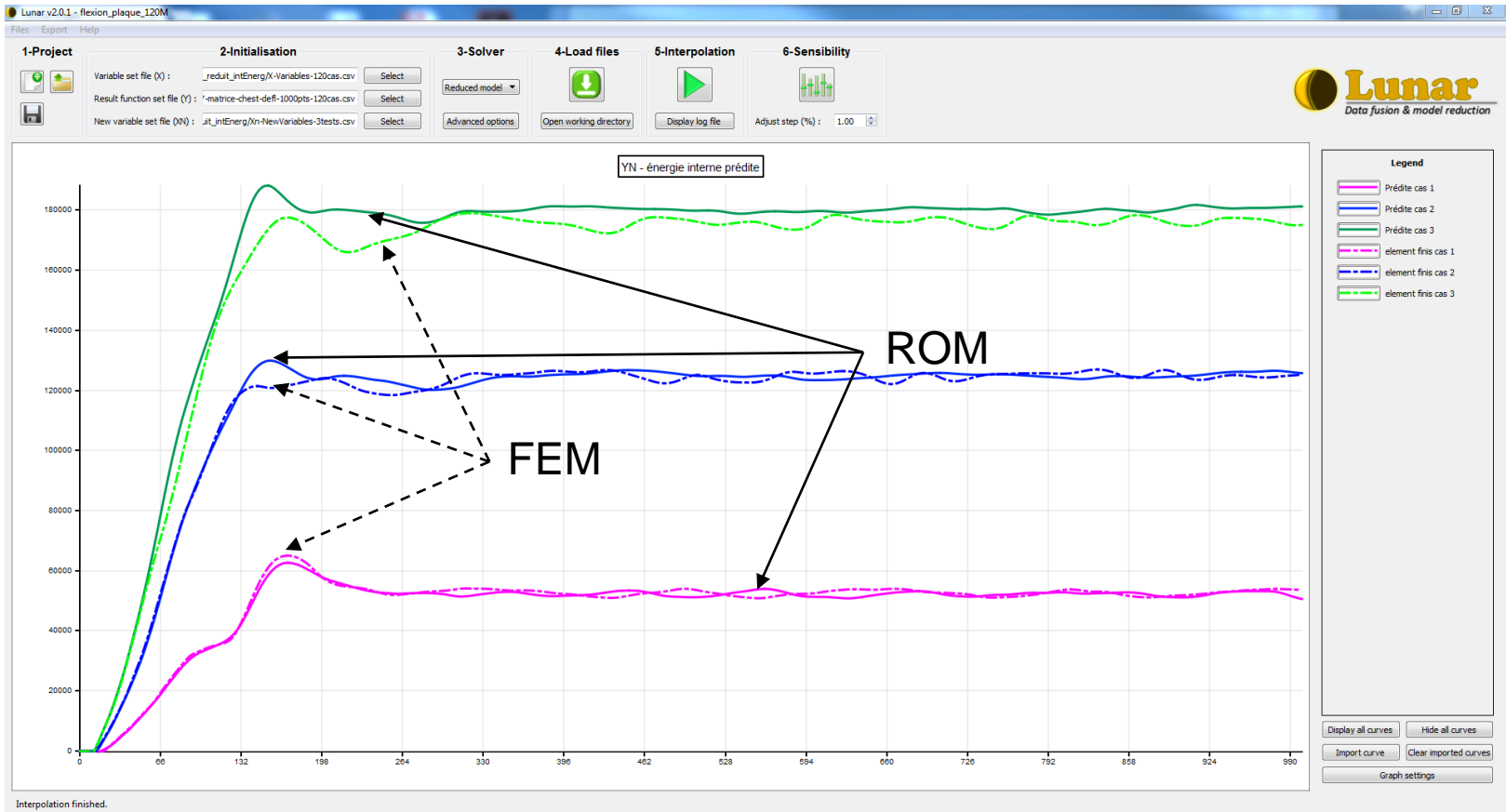
**Test 2** : New position

**Test 3** : New velocity; New velocity; New angle

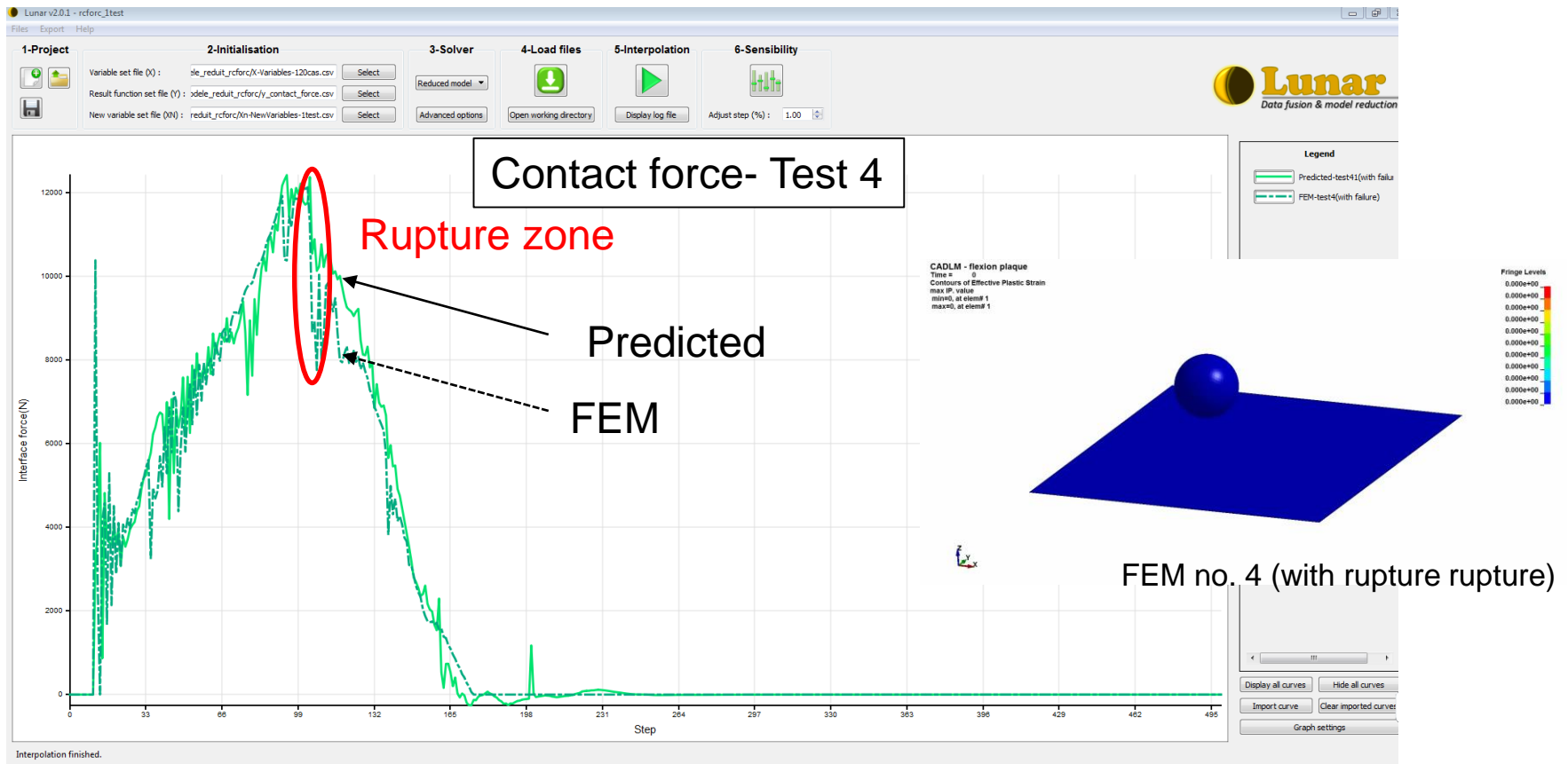
Mesure à prédire:

Y: internal energy versus time

# Example – plate impact



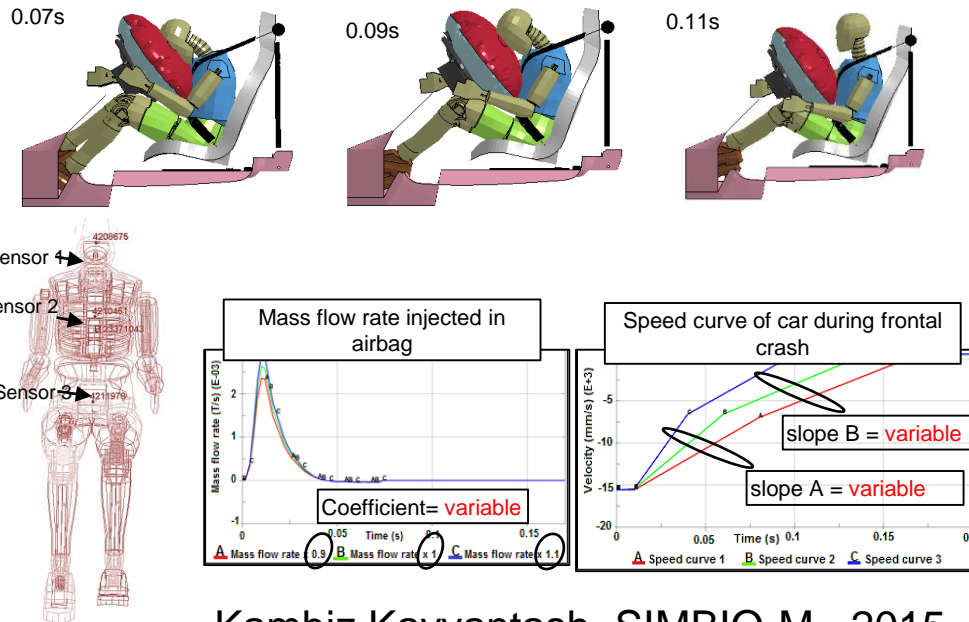
# Example – plate impact



# Example – Sled test

**Predict head, thorax and pelvis  
acceleration :  $a(t)$**   
**Predict thorax compression:  $d(t)$**

**X1: impact velocity : Slope A**  
**X2: impact velocity : Slope B**  
**X3: injected airbag mass debit (enthalpy)**

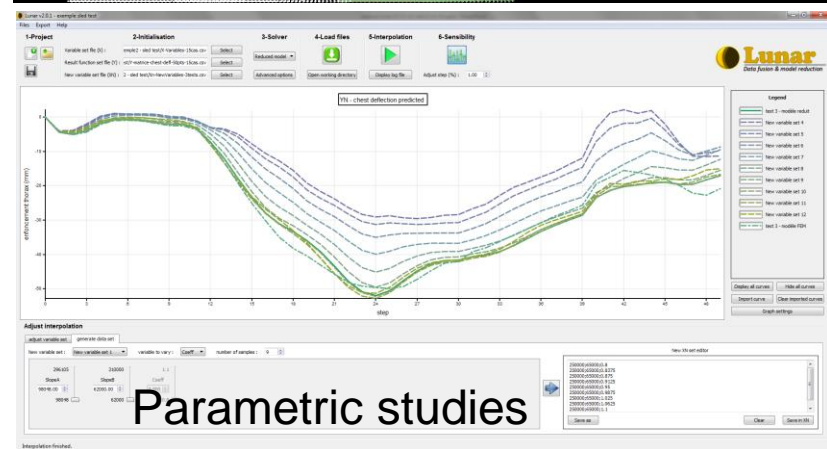
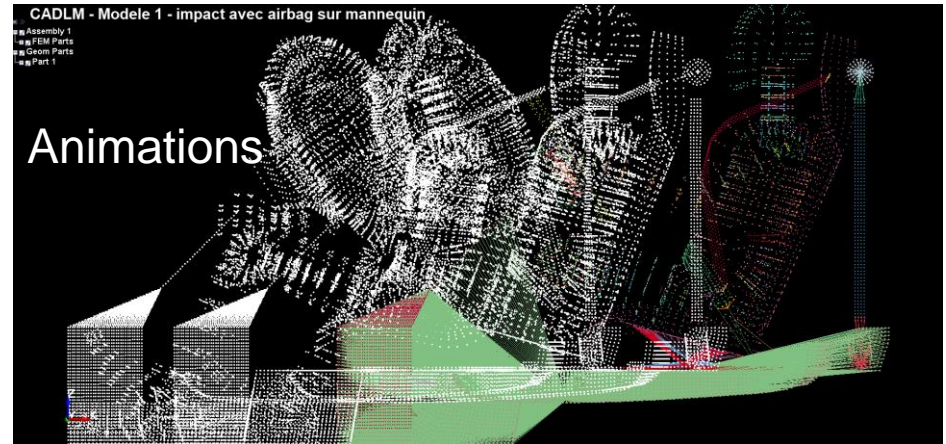
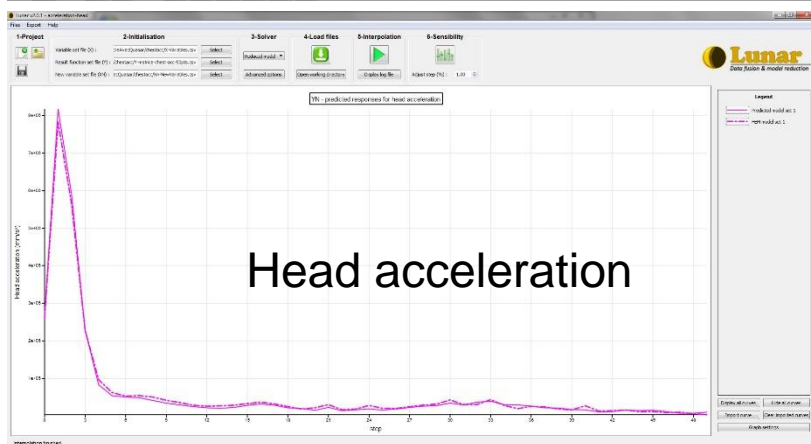
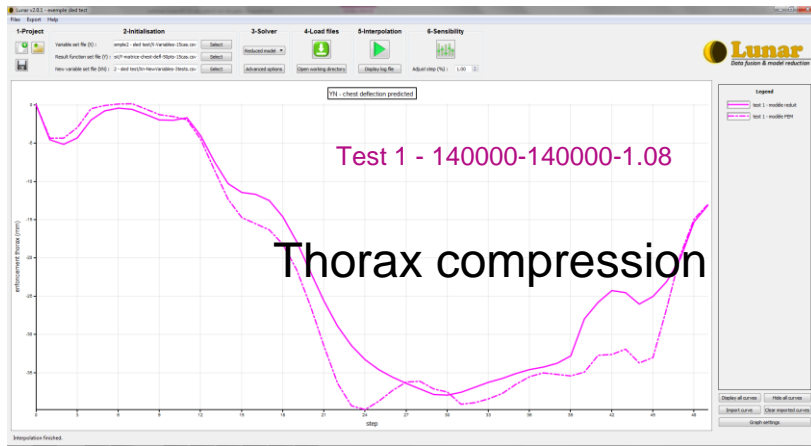


X1	X2	X3	Y1	Y2
Velocity Slope A	Velocity Slope B	Injected gas Coeff.	Chest deflection	Head Injury criteria
122285	83559	0.9	36	358
122285	83559	1	37	371
122285	83559	1.1	38	391
179679	88704	0.9	42	667
179679	88704	1	43	596
179679	88704	1.1	42	714
296105	118272	0.9	43	955
296105	118272	1	57	1076
296105	118272	1.1	58	1061
98048	189184	1.04	34.5	212
150000	310000	0.93	44.5	978
160800	62000	0.85	39	359
230000	230000	0.8	43	1413
116170	114475	0.902	34	279
189541	69353	0.84	37	420

Kambiz Kayvantash, SIMBIO-M , 2015



# Example – Sled test Predictions

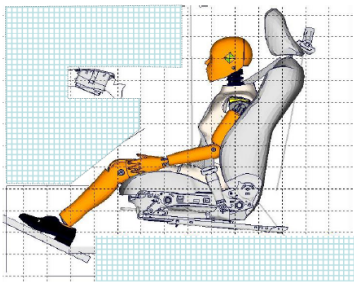




# Example – Validation of Nij with HII F50

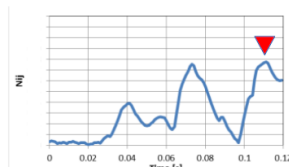
## Background

•Nij of HYBRID III AF05%ile dummy at passenger seat was studied by sled FE model. Timing of the maximum value of Nij depended on parameter of seat belt and airbag. Response surface method may not be applicable to optimize Nij in this case. ODYSSEE, developed by CADLM company and presented at 10th European LS-DYNA Conference, was applied to estimate time history of Nij.

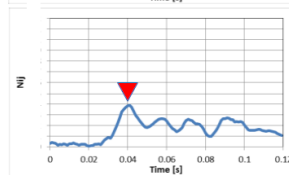


Sled FE model for NCAP

Integrated Safety



Case A: Small vent hole with weak force limiter



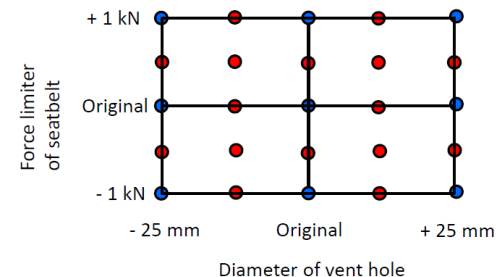
Case B: Medium vent hole with weak force limiter

Time history of Nij

TOYOTA

## Case study

- Force limiter of seatbelt and diameter of vent hole were parameters.
- Nine cases were sampled and simulated by FE model for generating reduced model.
- Sixteen cases were reconstructed by the reduce model and validated with results of FE model.



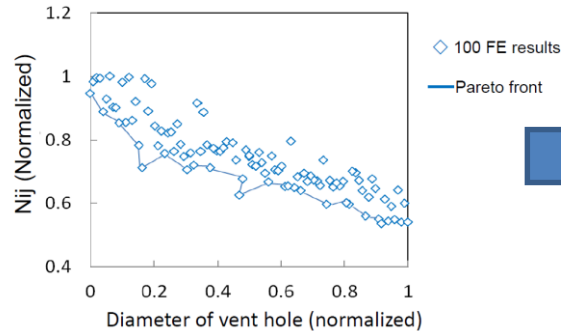
- :Sampled by FE model
- :Estimated by reduced model

Integrated Safety

TOYOTA

# Population Studies

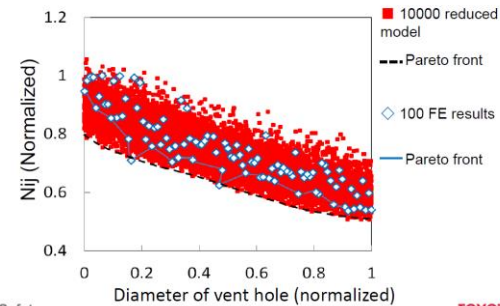
•100 FE results seemed be not enough to identify exact Pareto front curve.



Integrated Safety

TOYOTA

•10000 reduced model results showed smoother Pareto front curve than 100 FE results with CPU time of 10 seconds on PC.

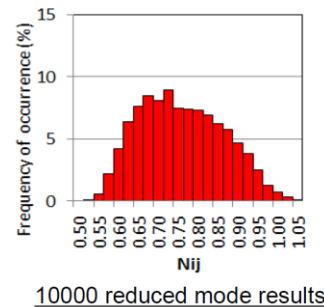
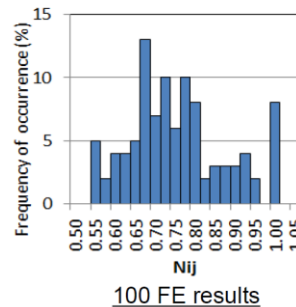


Integrated Safety

TOYOTA

## Frequency distribution of dummy injury scale

•10000 reduced model results showed more realistic frequency distribution than 100 FE results.



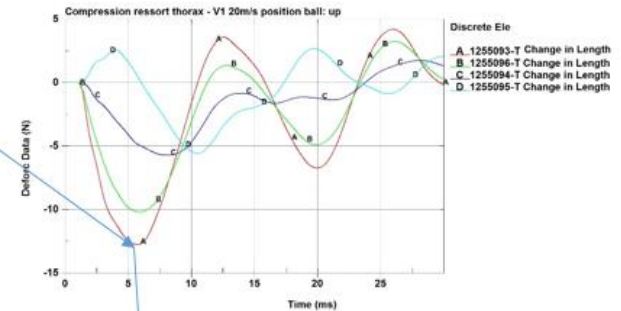
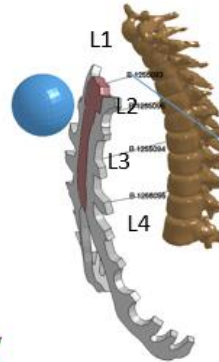
Courtesy of  
Toyota Motor Company,  
Tsuyoshi Yasuki,  
LS-DYNA conference 2018

# Example – Morphing + (personalized impact on thorax)

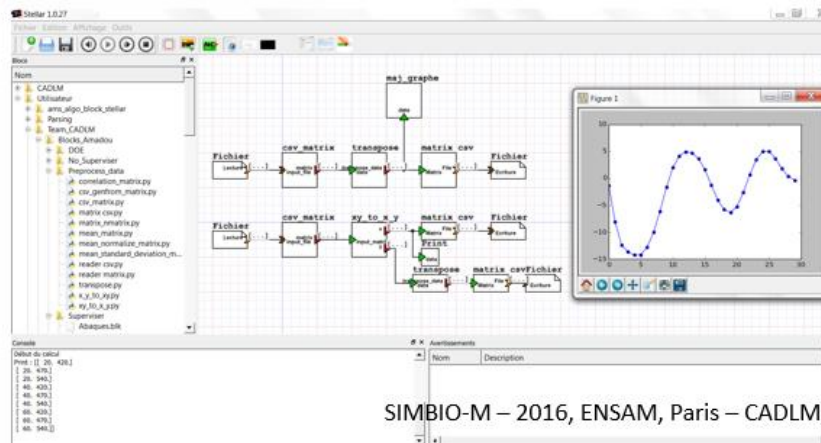
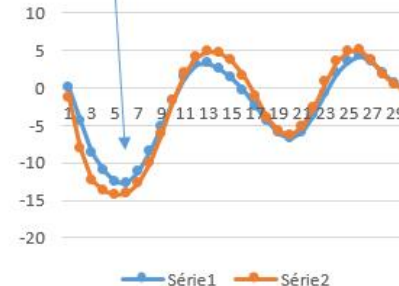
LS-DYNA keyword deck by LS-PrePost  
Time = 0



HUDYNI-Model



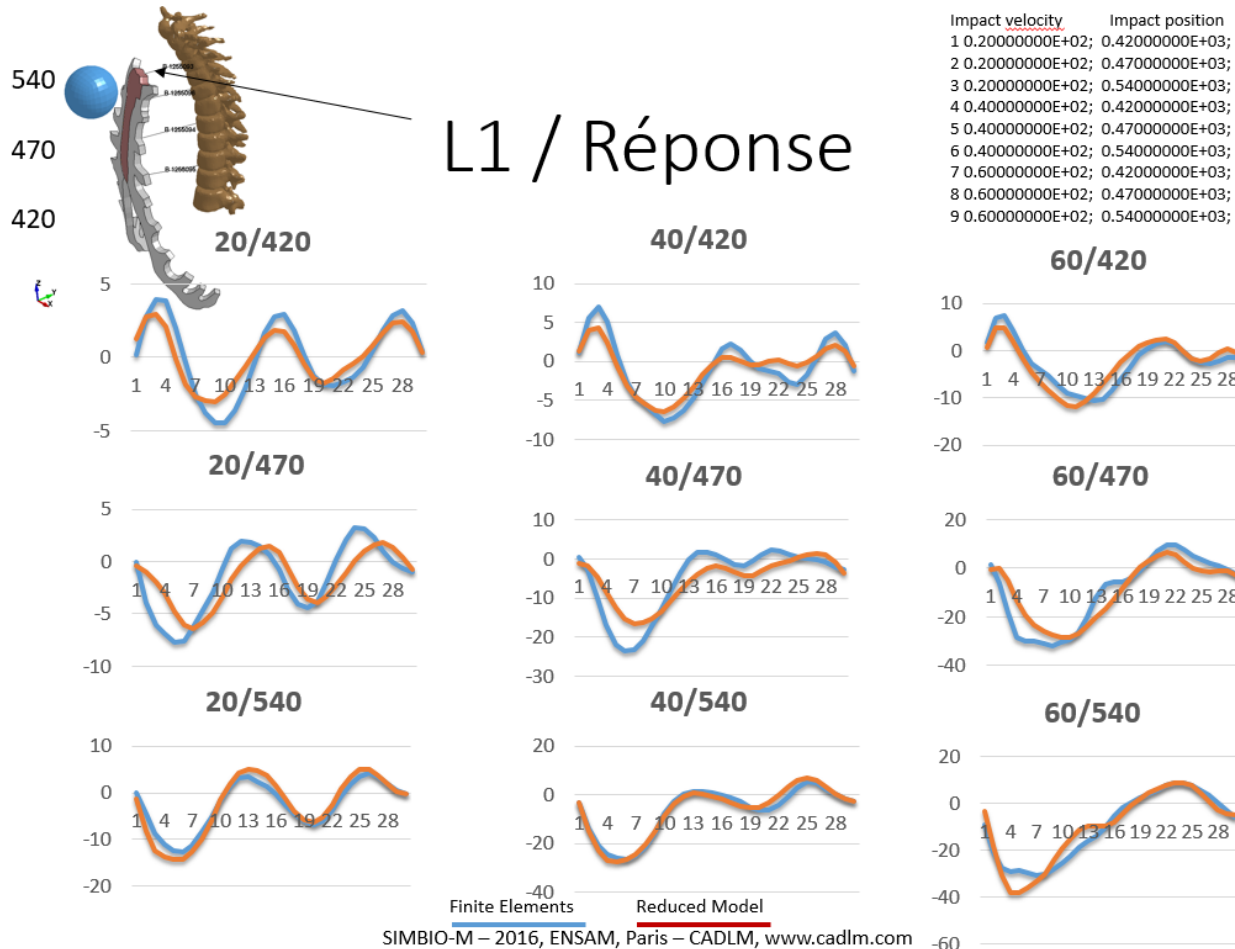
Finite Element vs Reduced Model



SIMBIO-M – 2016, ENSAM, Paris – CADLM, [www.cadlm.com](http://www.cadlm.com)



# Biomechanics - Predicted results



SIMBIO-M – 2016, ENSAM, Paris – CADLM, [www.cadlm.com](http://www.cadlm.com)



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